

12/PRTS

DESCRIPTION

AZIMUTH MEASURING DEVICE AND AZIMUTH MEASURING METHOD

5 Technical Field

The present invention relates to an azimuth measuring device and azimuth measuring method, and is preferably applicable to offset corrections of a magnetic sensor in particular.

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Background Art

15 An azimuth measuring device which arranges magnetic sensors in two or three directions, measures earth magnetism using the magnetic sensors in the respective directions and measures azimuth is known.

When a magnetized part such as a speaker is placed near the magnetic sensors of such an azimuth measuring device, an offset is produced in the outputs of the magnetic sensors due to a magnetic field leaking from the magnetized part.

20 In order to prevent errors from occurring in azimuth calculations due to the offset of the magnetic sensors, the above described azimuth measuring device needs to carry out calibration on the azimuth measuring device for the purpose of correcting the offset of the magnetic sensors.

25 Therefore, a conventional azimuth measuring device carries out calibration on the azimuth measuring device, for example, by rotating the azimuth measuring device around a specific axis at a constant angular velocity.

Figure 12 illustrates an output waveform of a magnetic sensor when an azimuth measuring device is rotated around the z-axis at a constant angular velocity.

In Figure 12, when a portable device 301 is rotated around the z-axis at a constant angular velocity ω , an output S_{rx} of an x-axis Hall element HE_x mounted on the portable device 301 is given by Formula (1) below:

$$S_{rx} = a_x M_{xy} \cos(\omega t + \theta_0) + X_0 \quad \dots (1)$$

where a_x is sensitivity of the x-axis Hall element HE_x and X_0 is an offset of the x-axis Hall element HE_x .

Furthermore,

$$M_{xy} = \sqrt{M_x^2 + M_y^2}$$

$$\theta_0 = \tan^{-1}(M_y/M_x)$$

where M_x is an x-direction component of earth magnetism M and M_y is a y-direction component of earth magnetism M .

Therefore, a maximum value X_{\max} and minimum value X_{\min} of the output S_{rx} of the x-axis Hall element HE_x can be expressed by Formulas (2), (3) below:

$$X_{\max} = a_x M_{xy} + X_0 \quad \dots (2)$$

$$X_{\min} = -a_x M_{xy} + X_0 \quad \dots (3)$$

As a result, from Formulas (2), (3), the offset X_0 of the x-axis Hall element HE_x can be calculated by Formula (4) below:

$$X_0 = (X_{\max} + X_{\min}) / 2 \quad \dots (4)$$

Figure 13 is a flow chart showing a conventional azimuth measuring method.

In Figure 13, a calibration start button of the portable device 301 is pressed (step S21).

Then, while keeping the portable device 301 mounted with the x-axis Hall element HEx horizontal, the portable device 301 is slowly rotated 360 degrees at a constant speed (step S22).

5 After the portable device 301 is rotated 360 degrees, the calibration end button of the portable device 301 is pressed (step S23).

 Here, while the portable device 301 is rotated 360 degrees, a maximum value X_{\max} and minimum value X_{\min} of the output Srx
10 of the x-axis Hall element HEx are searched, a value obtained by adding up these values and then dividing by 2 is assumed to be an offset X_0 of the x-axis, and thus it is possible to carry out calibration of the x-axis.

 However, according to the conventional azimuth measuring
15 method, it is necessary to rotate the portable device 301 360 degrees or more on a specific plane to search the maximum value X_{\max} and minimum value X_{\min} of the output Srx of the x-axis Hall element HEx.

 As a result, there are problems that when the rotation
20 speed of the portable device 301 does not fall within a certain speed range, the calibration accuracy deteriorates, for example, when the rotation speed of the portable device 301 is too high, the maximum value X_{\max} and minimum value X_{\min} may be overlooked and when the rotation speed is too low, the amount
25 of data read becomes enormous, causing a memory to overflow.

 For this reason, the user is required to repeat trial and error and rotate the portable device 301 many times until calibration is completed successfully.

Therefore, it is an object of the present invention to provide an azimuth measuring device and azimuth measuring method capable of carrying out calibration on magnetic sensors without putting load on the user.

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Disclosure of the Invention

In order to attain the above-described object, the azimuth measuring device according to claim 1 of the present invention comprises earth magnetism detection means with 2 or 3 axes for detecting earth magnetism, output data acquisition means for acquiring 2-axis output data when the orientation of the earth magnetism detection means changes while keeping the detection directions of the two axes on a predetermined plane or 3-axis output data when the orientation of the earth magnetism detection means changes in a three-dimensional space repeatedly a predetermined number of times or more, reference point estimation means for defining a reference point on a two-dimensional coordinate system whose coordinate values correspond to the 2-axis output data or on a three-dimensional coordinate system whose coordinate values correspond to the 3-axis output data and estimating the coordinates of reference point using a statistical technique so that a variation in the distance from the 2-axis or 3-axis output data group acquired by the output data acquisition means to the reference point becomes a minimum, and offset information calculation means for calculating offset information with respect to the output data of the earth magnetism detection means based on the coordinates of reference point.

By so doing, simply changing the orientation of the measuring device on a predetermined plane arbitrarily or three-dimensionally arbitrarily allows offset information of the detection means with respect to each axis output to be
5 calculated.

Here, calculating offset information simply requires the orientation of the measuring device to be changed and the range in which the orientation changes may be limited. For example, when the 2-axis earth magnetism detection means is provided,
10 that range may be less than 180 degrees or less than 90 degrees or when the 3-axis earth magnetism detection means is provided, that range may be less than 2π or less than π of solid angle. The position may be changed when the orientation of the measuring device changes.

15 Thus, the offset can be calibrated without orienting the measuring device to a specified direction or rotating the measuring device at a predetermined speed, reducing the load of offset calibration work on the user.

Furthermore, even if the offset values change drastically
20 due to temperature variation, etc., the user need not repeat offset calibration consciously, and offset calibration is performed automatically while the user is performing normal azimuth measurement, making it possible to reduce load on the user.

25 Furthermore, the azimuth measuring device according to claim 2 of the present invention is the azimuth measuring device according to claim 1, wherein the reference point estimation means comprises coefficients and constant term calculation

means for calculating coefficients and constant terms of simultaneous linear equations whose unknowns are the coordinates of reference from the 2-axis or 3-axis output data group and simultaneous linear equation analysis means for
5 estimating the coordinates of reference point by calculating solutions to the simultaneous linear equations including the coefficients and constant terms.

This makes it possible to, without increases in the calculation time by increasing the number of acquired output
10 data pieces and using statistical technique, accurately estimate the reference point and increase the offset calibration accuracy.

Furthermore, the azimuth measuring device according to claim 3 is the azimuth measuring device according to claim
15 1, wherein the earth magnetism detection means is 3-axis earth magnetism detection means, and when a degree of the variation of the output data group is a predetermined value or below with respect to the output data group of the axis whose degree of variation is a minimum out of the 3-axis output data group,
20 the reference point estimation means defines a reference point on a two-dimensional coordinate system whose coordinate values correspond to the 2-axis output data for the 2-axis output data group which is generated by excluding the output data group of the axis whose degree of variation is a minimum from
25 the 3-axis output data group and estimates the coordinates of reference point from the 2-axis output data group.

In the azimuth measuring device according to the present invention, when 3-axis output data in the case where the

orientation of the earth magnetism detection means is changed in the three-dimensional space is acquired repeatedly a predetermined number of times or more by moving or rotating the azimuth measuring device using the 3-axis output data, if the azimuth measuring device is moved or rotated only on the plane perpendicular to any one of the three axes of the earth magnetism detection means (hereinafter referred to as "specific axis" in this paragraph), the output data of the specific axis hardly changes. For this reason, if the coordinates of reference point are estimated from the 3-axis output data group including the output data group of the specific axis, the exact coordinates of reference point may not be obtained. In this case, the exact value can be obtained by rather estimating the coordinates of reference point from the 2-axis output data group except the output data group of the specific axis.

Thus, even when the azimuth measuring device is moved or rotated only on the plane perpendicular to any one of the three axes of the earth magnetism detection means, it is possible to estimate the coordinates of reference point relatively accurately.

The azimuth measuring device according to claim 4 of the present invention is the azimuth measuring device according to claim 1, wherein the reference point estimation means comprises first difference calculation means for calculating a difference between a maximum value and minimum value of output data in the output data group of each axis from the 2-axis or 3-axis output data group and first difference decision means

for deciding whether the difference calculated by the first difference calculation means is equal to or greater than a predetermined value or not, and the reference point estimation means uses the 2-axis or 3-axis output data group for estimating
5 the reference point only when the difference calculated by the first difference calculation means is equal to or greater than a predetermined value.

Thus, when the orientation of the portable device is stationary or changes only a little, it is possible to prevent
10 the coordinates of reference point from being calculated with large errors and improve the accuracy in calculating the coordinates of reference point and keep the accuracy of offset calibration high.

Furthermore, the azimuth measuring device according to
15 claim 5 of the present invention is the azimuth measuring device according to claim 1, wherein the offset information calculation means comprises variation calculation means for calculating a variation at a predetermined number of the latest reference points calculated by the reference point estimation
20 means, and the offset information calculation means discards the reference point calculated by the reference point estimation means based on the calculation result of the variation calculation means.

Thus, when large errors are included in detected output
25 of earth magnetism due to noise, etc., or especially when the orientation of the 2-axis earth magnetism detection means is deviated from a predetermined plane, it is possible to prevent

wrong offset values from being calculated and inappropriate offset correction from being made.

Furthermore, the azimuth measuring device according to claim 6 of the present invention is the azimuth measuring device
5 according to claim 5, wherein the variation calculation means calculates the difference between the two latest reference points calculated by the reference point estimation means.

Furthermore, the azimuth measuring device according to claim 7 of the present invention is the azimuth measuring device
10 according to claim 1, further including second variation calculation means for calculating a variation at a predetermined number of the latest reference points calculated by the reference point estimation means and acceptability information creation means for creating acceptability
15 information regarding the acceptability of the offset information based on the calculation result of the second variation calculation means.

According to this structure, the second variation calculation means calculates a variation at a predetermined
20 number of the calculated latest reference points and the acceptability information creation means creates acceptability information based on the calculation result of the variation.

This allows the user to recognize the acceptability of
25 the offset information with reference to the acceptability information.

Furthermore, the azimuth measuring device according to claim 8 of the present invention is the azimuth measuring device

according to claim 7, wherein the acceptability information creation means divides the degree of acceptability of the offset information into a plurality of categories, classifies the offset information into any one of the categories according to the degree of variation calculated by the second variation calculation means and displays the degree of acceptability corresponding to the category.

According to this structure, the acceptability information creation means classifies the offset information into any one of the categories according to the calculated degree of variation and creates acceptability information indicating the degree of acceptability corresponding to the category.

Thus, it is possible to obtain the degree of acceptability (e.g., degree of acceptability such as excellent, good, fair) corresponding to each category, and thereby further facilitate the recognition of the acceptability of the offset information.

Furthermore, the azimuth measuring device according to claim 9 of the present invention is the azimuth measuring device according to claim 1, wherein the offset information calculation means comprises distance calculation means for calculating the distance from the output data group to the reference point and distance decision means for deciding whether the distance calculated by the distance calculation means is outside a predetermined range or not, and the offset information calculation means discards the output data group when the distance calculated by the distance calculation means is outside the predetermined range.

According to this structure, the distance calculation means calculates the distance from the output data group to the reference point and the distance decision means decides whether the calculated distance is outside the predetermined
5 range or not. Then, when the calculated distance is outside the predetermined range, the output data is discarded.

Thus, when a static external environment magnetic field exists or when earth magnetism is shielded, it is possible to prevent azimuth from being measured though earth magnetism
10 has not been detected correctly.

Furthermore, the azimuth measuring device according to claim 10 of the present invention is the azimuth measuring device according to claim 1, further including second distance calculation means for calculating the distance from the output
15 data group to the reference point and reliability information creation means for creating reliability information regarding the reliability of the azimuth measurement result based on the distance calculated by the second distance calculation means.

20 According to this structure, the second distance calculation means calculates the distance from the output data group to the reference point and the reliability information creation means creates reliability information indicating the degree of reliability according to the calculated distance.

25 This allows the user to recognize the reliability of the azimuth measurement result with reference to the reliability information.

Furthermore, the azimuth measuring device according to claim 11 of the present invention is the azimuth measuring device according to claim 10, wherein the reliability information creation means divides the degree of reliability of the azimuth measurement result into a plurality of categories, compares the distance calculated by the second distance calculation means with a plurality of thresholds, classifies the distance into any one of the categories and displays the degree of reliability corresponding to the category.

According to this structure, the reliability information creation means compares the calculated distance with a plurality of thresholds, classifies the distance into any one of the categories and creates reliability information indicating the degree of reliability corresponding to the category.

Thus, it is possible to obtain a degree of reliability corresponding to each category (e.g., degree of reliability such as excellent, good and fair), which further facilitates the recognition of the reliability of the azimuth measurement result.

Furthermore, the azimuth measuring device according to claim 12 of the present invention is the azimuth measuring device according to claim 1, wherein the data output acquisition means comprises third difference calculation means for calculating a difference between the output data output from the earth magnetism detection means and a predetermined number of pieces of immediately preceding output

data acquired by the output data acquisition means or the output
data output immediately before from the earth magnetism
detection means and third difference decision means for
deciding whether the difference calculated by the third
5 difference calculation means is smaller than a predetermined
value or not, and the output data acquisition means does not
acquire but discards the output data output from the earth
magnetism detection means when the difference calculated by
the third difference calculation means is smaller than the
10 predetermined value.

Thus, even if a state in which the orientation of the
portable device hardly changes during calibration continues,
it is possible to prevent a wrong offset value from being
calculated and an inappropriate offset correction from being
15 performed.

On the other hand, in order to attain the above described
object, the azimuth measuring method according to claim 13
of the present invention comprises a step of changing detection
directions of two axes for measurement of earth magnetism while
20 keeping the detection directions of two axes on a predetermined
plane or changing the detection directions of three axes in
a three-dimensional space, a step of acquiring the 2-axis or
3-axis output data for measurement of earth magnetism when
the detection directions change, a step of deciding whether
25 the output data is acquired a predetermined number of times
or more or not, a step of defining a reference point on a
two-dimensional coordinate system whose coordinate values
correspond to the 2-axis output data or on a three-dimensional

coordinate system whose coordinate values correspond to the 3-axis output data and estimating the coordinates of reference point using a statistical technique so that a variation in the distance from the output data group consisting of the 2-axis or 3-axis output data acquired the predetermined number of times or more to the reference point becomes a minimum and a step of calculating offset values with respect to the 2-axis or 3-axis output data based on the estimated the coordinates of reference point.

Thus, by only arbitrarily changing the orientation of the portable device on a predetermined plane or arbitrarily changing the orientation of the portable device three-dimensionally, it is possible to calculate an offset value with respect to the measurement result of the earth magnetism and calibrate the offset.

This allows the user to realize offset calibration without the user being aware of the offset calibration, making it possible to reduce load on the user in calibrating the offset.

Furthermore, the azimuth measuring method according to claim 14 of the present invention is the azimuth measuring method according to claim 13, wherein the step of estimating the coordinates of reference point comprises a step of calculating coefficients and constant terms of simultaneous linear equations whose unknowns are the coordinates of reference point from the 2-axis or 3-axis output data group and a step of calculating solutions to the simultaneous linear equations including the coefficients and constant terms and estimating the coordinates of reference point.

Furthermore, the azimuth measuring method according to claim 15 of the present invention is the azimuth measuring method according to claim 13, wherein the step of changing the detection direction is intended to change detection
5 directions of three axes in a three-dimensional space and the step of estimating the coordinates of reference point comprises a step of calculating the degree of variation of output data of the output data group of each axis of the 3-axis output data group and obtaining the axis corresponding to the minimum
10 degree of variation and a minimum value of the degree of variation, a step of deciding whether the minimum value of the degree of variation is equal to or lower than a predetermined value or not and a step of defining, when the minimum value of the degree of variation is equal to or lower than the
15 predetermined value, a reference point on a two-dimensional coordinate system whose coordinate values correspond to the 2-axis output data for the 2-axis output data group wherein the output data group of the axis whose degree of variation becomes a minimum is excluded from the 3-axis output data group
20 and estimating the coordinates of reference point from the 2-axis output data group.

Furthermore, the azimuth measuring method according to claim 16 of the present invention is the azimuth measuring method according to claim 13, wherein the step of estimating
25 the coordinates of reference point comprises a step of calculating the difference between a maximum value and minimum value of output data of the output data group of each axis of the output data group, a step of deciding whether the

difference between the maximum value and minimum value is equal to or greater than a predetermined value or not and a step of estimating the coordinates of reference point when the difference between the maximum value and minimum value is equal
5 to or greater than the predetermined value.

Furthermore, the azimuth measuring method according to claim 17 of the present invention is the azimuth measuring method according to claim 13, wherein the step of calculating offset values with respect to the 2-axis or 3-axis output data
10 comprises a step of calculating a variation at a predetermined number of the latest reference points calculated in the step of estimating the coordinates of reference point and a step of discarding the reference point calculated in the step of estimating the coordinates of reference point based on the
15 calculation result of the variation.

Furthermore, the azimuth measuring method according to claim 18 of the present invention is the azimuth measuring method according to claim 13, further including a step of calculating a variation at a predetermined number of the
20 estimated latest coordinates of reference points and a step of creating acceptability information regarding the acceptability of the offset values calculated in the step of calculating the offset values based on the calculation result of the variation.

25 Furthermore, the azimuth measuring method according to claim 19 of the present invention is the azimuth measuring method according to claim 13, wherein the step of calculating offset values with respect to the 2-axis or 3-axis output data

comprises a step of calculating the distance from the output data group to the reference point, a step of deciding whether the distance from the output data group to the reference point is outside a predetermined range or not and a step of discarding the output data group when the distance from the output data group to the reference point is outside the predetermined range.

Furthermore, the azimuth measuring method according to claim 20 of the present invention is the azimuth measuring method according to claim 13, further including a step of calculating the distance from the output data group to the reference point and a step of creating reliability information regarding the reliability of the azimuth measurement result based on the distance calculation result.

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Brief Description of the Drawings

Figure 1 is a perspective view showing an overall structure of a portable device according to an embodiment of the present invention. Figure 2 is a block diagram showing a schematic structure of an azimuth measuring device according to an embodiment of the present invention. Figure 3 illustrates a concept of an azimuth measuring method for an offset value according to an embodiment of the present invention. Figure 4 is a flow chart showing an azimuth measuring method for an offset value according to an embodiment of the present invention. Figure 5 is a perspective view showing an overall structure of a portable device according to an embodiment with two axes. Figure 6 is a block diagram showing an overall

structure of an azimuth measuring device according to an embodiment with two axes;

Figure 7 illustrates a concept of an azimuth measuring method for an offset value according to an embodiment with two axes. Figure 8 is a flow chart showing an azimuth measuring method for an offset value according to an embodiment with two axes. Figure 9 is a graph showing a variation on the time axis of S_x , S_y , S_z data acquired when the orientation of the portable device changes appropriately. Figure 10 is a graph showing a variation on the time axis of S_x , S_y , S_z data acquired when the orientation of the portable device hardly changes. Figure 11 is a graph showing a variation on the time axis of S_x , S_y , S_z data when the orientation of the portable device changes only for a short time when the S_x , S_y , S_z data is being acquired;

Figure 12 illustrates an output waveform of a magnetic sensor when an azimuth measuring device is rotated around the z-axis at a constant angular velocity. Figure 13 is a flow chart showing an azimuth measuring method of a conventional azimuth measuring device.

Best Mode for Carrying Out the Invention

With reference now to the attached drawings, an azimuth measuring device and azimuth measuring method according to embodiments of the present invention will be explained below.

Figure 1 is a perspective view showing an overall structure of a portable device according to an embodiment of the present invention.

In Figure 1, a portable device 201 is provided with a display section 202 and an antenna 203 and incorporates an azimuth measuring device which measures earth magnetism on three axes to obtain azimuth.

5 Here, the azimuth measuring device is provided with an x-axis Hall element H_{Ex} which measures an x-direction component M_x of earth magnetism M , a y-axis Hall element H_{Ey} which measures a y-direction component M_y of earth magnetism M and a z-axis Hall element H_{Ez} which measures a z-direction component M_z of earth magnetism M , and the x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} are arranged in such a way that their respective magnetism sensitive surfaces are perpendicular to the respective axes.

Figure 2 is a block diagram showing a schematic structure of an azimuth measuring device according to an embodiment of the present invention.

In Figure 2, the azimuth measuring device is provided with a three-axis magnetic sensor 11, a magnetic sensor drive power supply section 12, a chopper section 13, a differential input amplifier 14, an A/D conversion section 15, a correction calculation section 16, an azimuth calculation section 17, an offset information calculation section 18, an offset information storage section 19a and a sensitivity correction information storage section 19b, and the three-axis magnetic sensor 11 is provided with an x-axis Hall element H_{Ex} , a y-axis Hall element H_{Ey} and a z-axis Hall element H_{Ez} .

The x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} are intended to detect earth magnetism

and are preferably made of compound semiconductor such as InSb, InAs and GaAs or based on Si monolithic.

The chopper section 13 is intended to switch between terminals for driving the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz, applies a drive voltage output from the magnetic sensor drive power supply section 12 to the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz and outputs the signals output from the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz to the differential input amplifier 14 in a time-sharing manner.

Here, the chopper section 13 can use 90° chopper drive or 360° chopper drive, etc. When driving the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz, the 90° chopper drive can cancel most of the offset terms of the Hall elements themselves included in the outputs of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz.

The 360° chopper drive can not only cancel the offset terms of the Hall elements themselves included in the outputs of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz but also easily cancel an electric offset term of the following differential input amplifier 14 itself.

The signals output from the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz are amplified by the differential input amplifier 14, the output value amplified here is converted to a digital signal by the A/D

conversion section 15 and then input to the correction calculation section 16.

Here, the amplified output value S_{rx} of the x-axis Hall element HE_x can be expressed by Formula (5) below, the amplified output value S_{ry} of the y-axis Hall element HE_y can be expressed by Formula (6) below and the amplified output value S_{rz} of the z-axis Hall element HE_z can be expressed by Formula (7) below.

$$S_{rx} = a_x \cdot M_x + C_{rx} \quad \dots (5)$$

10 $S_{ry} = a_y \cdot M_y + C_{ry} \quad \dots (6)$

$$S_{rz} = a_z \cdot M_z + C_{rz} \quad \dots (7)$$

where a_x is sensitivity of the x-axis Hall element HE_x , C_{rx} is an offset of the x-axis Hall element HE_x , a_y is sensitivity of the y-axis Hall element HE_y , C_{ry} is an offset of the y-axis Hall element HE_y , a_z is sensitivity of the z-axis Hall element HE_z , C_{rz} is an offset of the z-axis Hall element HE_z , M_x is an x-direction component of earth magnetism M , M_y is a y-direction component of earth magnetism M , and M_z is a z-direction component of earth magnetism M .

20 The offset information storage section 19a stores the offsets of the x-axis Hall element HE_x , y-axis Hall element HE_y and z-axis Hall element HE_z and the sensitivity correction information storage section 19b stores sensitivity correction information for correcting variations in sensitivity of the
25 x-axis Hall element HE_x , y-axis Hall element HE_y and z-axis Hall element HE_z .

When azimuth measurement is in progress, the correction calculation section 16 corrects the amplified output values

Srx, Sry, Srz of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz using the offset information and sensitivity correction information, picks up only the x, y, z-axis components Mx, My, Mz of earth magnetism M and outputs
5 these components to the azimuth calculation section 17.

The azimuth calculation section 17 calculates azimuth θ based on the signs of the x, y, z-axis components Mx, My, Mz of earth magnetism M and Formula $\theta = \tan^{-1}(My/Mx)$.

When offset calibration is in progress, the amplified
10 output values Srx, Sry, Srz of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz are output to the offset information calculation section 18.

When the orientation of the portable device 201 is arbitrarily changing in a three-dimensional space, the offset
15 information calculation section 18 acquires the amplified output values Srx, Sry, Srz of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz a predetermined number of times or more and corrects sensitivity based on the sensitivity correction information stored in the
20 sensitivity correction information storage section 19b.

Here, the amplified output value Sx of the x-axis Hall element HEx, amplified output value Sy of the y-axis Hall element HEy and amplified output value Sz of the z-axis Hall element HEz after the sensitivity correction can be expressed
25 by Formulas (8), (9) and (10) below:

$$Sx = a_0/a_x \cdot Srx = a_0 \cdot Mx + Cx \quad \dots (8)$$

$$Sy = a_0/a_y \cdot Sry = a_0 \cdot My + Cy \quad \dots (9)$$

$$Sz = a_0/a_z \cdot Srz = a_0 \cdot Mz + Cz \quad \dots (10)$$

where a_0/a_x is a sensitivity correction coefficient of the x-axis Hall element H_{Ex} , a_0/a_y is a sensitivity correction coefficient of the y-axis Hall element H_{Ey} , a_0/a_z is a sensitivity correction coefficient of the z-axis Hall element H_{Ez} and a_0 is sensitivity after the sensitivity corrections of the x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} .

Furthermore, C_x is an offset after the sensitivity correction of the x-axis Hall element H_{Ex} , C_y is an offset after the sensitivity correction of the y-axis Hall element H_{Ey} and C_z is an offset after the sensitivity correction of the z-axis Hall element H_{Ez} , and

$$C_x = a_0/a_x \cdot C_{rx}$$

$$C_y = a_0/a_y \cdot C_{ry}$$

$$15 \quad C_z = a_0/a_z \cdot C_{rz}$$

When the amplified output values S_x , S_y , S_z are arranged on an xyz coordinate system as the x, y, z components respectively, the offset information calculation section 18 estimates the coordinates of a reference point whose distances from the respective points become as equal as possible.

The offset information storage section 19a stores the x component of the coordinates of this reference point as a current offset C_x of the x-axis Hall element H_{Ex} , the y component of the center coordinates of this sphere as a current offset C_y of the y-axis Hall element H_{Ey} and the z component of the center coordinates of this sphere as a current offset C_z of the z-axis Hall element H_{Ez} .

Since sensitivity of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz hardly changes when the portable device 201 is in use, the sensitivity correction information on the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz may be stored only once when the portable device 201 is manufactured.

Figure 3 illustrates the concept of the azimuth measuring method for an offset value according to an embodiment of the present invention.

In Figure 3, the orientation of the portable device 201 is changed arbitrarily in a three-dimensional space and the amplified output value Sx of the x-axis Hall element HEx, amplified output value Sy of the y-axis Hall element HEy and the amplified output value Sz of the z-axis Hall element HEz are acquired repeatedly in the meantime. Then, as shown in Figure 3, in the xyz space in which Sx, Sy, Sz correspond to the x, y, z-axis direction components, the repeatedly acquired Sx, Sy, Sz data are arranged as P₁(S_{1x}, S_{1y}, S_{1z}), P₂(S_{2x}, S_{2y}, S_{2z}), P₃(S_{3x}, S_{3y}, S_{3z}), ...

Here, when Formulas (8), (9), (10) are modified as follows:

$$\frac{S_x - C_x}{a_0} = M_x \quad (11)$$

$$\frac{S_y - C_y}{a_0} = M_y \quad (12)$$

$$\frac{S_z - C_z}{a_0} = M_z \quad (13)$$

On the other hand, the relationship between Mx, My, Mz and earth magnetism M is:

$$M = \sqrt{M_x^2 + M_y^2 + M_z^2} \quad (14)$$

and earth magnetism M can be considered constant unless the location of the portable device 201 is changed drastically.

Thus, if

$$5 \quad r = a_0 \sqrt{M_x^2 + M_y^2 + M_z^2} \quad (15)$$

is assumed, the following formula holds:

$$(S_x - C_x)^2 + (S_y - C_y)^2 + (S_z - C_z)^2 = r^2 \quad (16)$$

That is, in the xyz space, $P_1(S1x, S1y, S1z)$, $P_2(S2x, S2y, S2z)$, $P_3(S3x, S3y, S3z)$, ... are all located at a constant distance
 10 r from a reference point $C1$ whose x, y, z -axis coordinate values consist of offsets Cx, Cy, Cz of the HEx, HEy, HEz .

Therefore, by estimating the reference point $C1$ from $P_1(S1x, S1y, S1z)$, $P_2(S2x, S2y, S2z)$, $P_3(S3x, S3y, S3z)$, ..., it is possible to obtain the offsets Cx, Cy, Cz of the HEx, HEy, HEz from the x, y, z -axis coordinate values of $C1$.
 15

There are various types of calculation methods to estimate $C1$ and $C1$ can be estimated by acquiring data at least four times. However, since the Sx, Sy, Sz data actually acquired are measured data of extremely feeble earth magnetism on the
 20 order of 0.01 mT and overlap with considerable noise, and therefore it is preferable to calculate $C1$ with the number of data pieces to be acquired set to 5 or 10 or more if possible using a statistical technique. Therefore, it is possible to estimate $C1$ accurately using the calculation method which will
 25 be described later using a statistical technique with an increase in the calculation time suppressed.

In the xyz space whose x, y, z-axis direction components consist of S_x , S_y , S_z respectively, the distance d_i from the S_x , S_y , S_z data $P_i(S_{ix}, S_{iy}, S_{iz})$ which has been acquired at the i th time to C_1 is as follows:

$$5 \quad d_i = \sqrt{(S_{ix} - C_x)^2 + (S_{iy} - C_y)^2 + (S_{iz} - C_z)^2} \quad (17)$$

By comparing Formula (17) with Formula (16) above, if the acquired S_x , S_y , S_z data don't overlap with noise and C_1 has been estimated ideally, d_i must be equal to r . However, both are not always equal, and therefore the difference between the square of d_i and the square of r is defined as a C_1 estimation error ϵ_i at $P_i(S_{ix}, S_{iy}, S_{iz})$ as shown in the following formula:

$$\begin{aligned} \epsilon_i &= d_i^2 - r^2 \\ &= (S_{ix} - C_x)^2 + (S_{iy} - C_y)^2 + (S_{iz} - C_z)^2 - r^2 \end{aligned} \quad (18)$$

Further, the square sum total of ϵ_i is defined as S expressed by the following formula.

$$\begin{aligned} S &= \sum \epsilon_i^2 \\ &= \sum \{ (S_{ix} - C_x)^2 + (S_{iy} - C_y)^2 + (S_{iz} - C_z)^2 - r^2 \}^2 \end{aligned} \quad (19)$$

Obtaining such C_x , C_y , C_z that minimize this square sum total S is appropriate as the estimation method.

When S becomes a minimum, the derivatives of S with respect to C_x , C_y , C_z and r are all considered to be 0. The respective derivatives become as follows:

$$\frac{\partial S}{\partial C_x} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_x} - C_x) \quad (20)$$

$$\frac{\partial S}{\partial C_y} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_y} - C_y) \quad (21)$$

$$\frac{\partial S}{\partial C_z} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_z} - C_z) \quad (22)$$

$$\frac{\partial S}{\partial r} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} \quad (23)$$

When all these derivatives become 0, the following formulas are obtained.

$$5 \quad \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_x} - C_x) = 0 \quad (24)$$

$$\sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_y} - C_y) = 0 \quad (25)$$

$$\sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 - r^2 \} (S_{i_z} - C_z) = 0 \quad (26)$$

$$\sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 \} - N r^2 = 0 \quad (27)$$

where N: number of data pieces acquired.

10 When Formula (27) above is solved with respect to r^2 , the formula becomes as follows:

$$r^2 = \frac{1}{N} \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 + (S_{i_z} - C_z)^2 \} \quad (28)$$

The following formulas are obtained by substituting Formula (28) into Formulas (24), (25) and (26) and rearranging

15 them:

$$\begin{aligned} C_x \sum S_{i_x} (S_{i_x} - \bar{S}_x) + C_y \sum S_{i_y} (S_{i_x} - \bar{S}_x) + C_z \sum S_{i_z} (S_{i_x} - \bar{S}_x) \\ = \frac{1}{2} \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2) (S_{i_x} - \bar{S}_x) \end{aligned} \quad (29)$$

$$\begin{aligned} C_x \sum S_{i_x} (S_{i_y} - \bar{S}_y) + C_y \sum S_{i_y} (S_{i_y} - \bar{S}_y) + C_z \sum S_{i_z} (S_{i_y} - \bar{S}_y) \\ = \frac{1}{2} \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2) (S_{i_y} - \bar{S}_y) \end{aligned} \quad (30)$$

$$\begin{aligned} C_x \sum S_{i_x} (S_{i_z} - \bar{S}_z) + C_y \sum S_{i_y} (S_{i_z} - \bar{S}_z) + C_z \sum S_{i_z} (S_{i_z} - \bar{S}_z) \\ = \frac{1}{2} \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2) (S_{i_z} - \bar{S}_z) \end{aligned} \quad (31)$$

where

$$\overline{S_x} = \frac{1}{N} \sum S_{i_x} \quad (32)$$

$$\overline{S_y} = \frac{1}{N} \sum S_{i_y} \quad (33)$$

$$\overline{S_z} = \frac{1}{N} \sum S_{i_z} \quad (34)$$

Formulas (29), (30) and (31) are expressed in matrix forms as follows:

$$\begin{bmatrix} \sum S_{i_x}(S_{i_x} - \overline{S_x}) & \sum S_{i_y}(S_{i_x} - \overline{S_x}) & \sum S_{i_z}(S_{i_x} - \overline{S_x}) \\ \sum S_{i_x}(S_{i_y} - \overline{S_y}) & \sum S_{i_y}(S_{i_y} - \overline{S_y}) & \sum S_{i_z}(S_{i_y} - \overline{S_y}) \\ \sum S_{i_x}(S_{i_z} - \overline{S_z}) & \sum S_{i_y}(S_{i_z} - \overline{S_z}) & \sum S_{i_z}(S_{i_z} - \overline{S_z}) \end{bmatrix} \begin{bmatrix} C_x \\ C_y \\ C_z \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2)(S_{i_x} - \overline{S_x}) \\ \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2)(S_{i_y} - \overline{S_y}) \\ \sum (S_{i_x}^2 + S_{i_y}^2 + S_{i_z}^2)(S_{i_z} - \overline{S_z}) \end{bmatrix} \quad (35)$$

5 Formula (35) above are simultaneous linear equations with respect to C_x, C_y, C_z and the solutions can be calculated using well known solutions to simultaneous linear equations such as UL decomposition. Therefore, it is possible to calculate C_x, C_y, C_z when S becomes a minimum while suppressing an increase
10 in the calculation time.

The following equations are also derived from Formula (35) above, and therefore a formula which is convenient for calculation of the solution can be selected.

$$\begin{aligned}
& \begin{bmatrix} \sum Si_x(Si_x - \overline{S_x}) & \sum Si_y(Si_x - \overline{S_x}) & \sum Si_z(Si_x - \overline{S_x}) \\ \sum Si_y(Si_x - \overline{S_x}) & \sum Si_y(Si_y - \overline{S_y}) & \sum Si_z(Si_y - \overline{S_y}) \\ \sum Si_z(Si_x - \overline{S_x}) & \sum Si_z(Si_y - \overline{S_y}) & \sum Si_z(Si_z - \overline{S_z}) \end{bmatrix} \begin{bmatrix} C_x \\ C_y \\ C_z \end{bmatrix} \\
& = \frac{1}{2} \begin{bmatrix} \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_x - \overline{S_x}) \\ \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_y - \overline{S_y}) \\ \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_z - \overline{S_z}) \end{bmatrix} \quad (36)
\end{aligned}$$

$$\begin{aligned}
& \begin{bmatrix} \sum Si_x^2 - \overline{NS_x^2} & \sum Si_x Si_y - \overline{NS_x S_y} & \sum Si_x Si_z - \overline{NS_x S_z} \\ \sum Si_x Si_y - \overline{NS_x S_y} & \sum Si_y^2 - \overline{NS_y^2} & \sum Si_y Si_z - \overline{NS_y S_z} \\ \sum Si_x Si_z - \overline{NS_x S_z} & \sum Si_y Si_z - \overline{NS_y S_z} & \sum Si_z^2 - \overline{NS_z^2} \end{bmatrix} \begin{bmatrix} C_x \\ C_y \\ C_z \end{bmatrix} \\
& = \frac{1}{2} \begin{bmatrix} \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_x - \overline{S_x}) \\ \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_y - \overline{S_y}) \\ \sum (Si_x^2 + Si_y^2 + Si_z^2)(Si_z - \overline{S_z}) \end{bmatrix} \quad (37)
\end{aligned}$$

Furthermore, if the number of data pieces acquired is increased and an estimation calculation of the reference point C1 is performed using the above described calculation method, the Sx, Sy, Sz data P₁(S1x, S1y, S1z), P₂(S2x, S2y, S2z), P₃(S3x, S3y, S3z),... repeatedly acquired in Figure 3 need not always be distributed in all directions when viewed from C1 and may also be limited to within a range of, for example, about 2π to π in terms of a solid angle. That is, the directions toward P₁(S1x, S1y, S1z), P₂(S2x, S2y, S2z), P₃(S3x, S3y, S3z),... viewed from C1 correspond to the orientations of the portable device 201 when the respective pieces of data are acquired, and therefore it is not necessary to orient the portable device 201 in all directions uniformly when an offset value is calibrated, and the orientations of the portable device 201 may be limited to within a range of, for example, about 2π to π in terms of a solid angle.

Figure 4 is a flow chart showing an azimuth measuring method for an offset value according to an embodiment of the present invention.

In Figure 4, the offset information calculation section 5 18 provides a data buffer for storing the amplified output value S_{rx} of the x-axis Hall element H_{Ex} , amplified output value S_{ry} of the y-axis Hall element H_{Ey} and amplified output value S_{rz} of the z-axis Hall element H_{Ez} , 10 values each (step S11).

10 Then, the offset information calculation section 18 acquires the amplified output values S_{rx} , S_{ry} , S_{rz} of the x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} , 10 values each (step S12, S13), multiplies the amplified output values S_{rx} , S_{ry} , S_{rz} of the x-axis Hall element 15 H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} by sensitivity correction coefficients respectively based on the sensitivity correction information stored in the sensitivity correction information storage section 19b to obtain amplified output values S_x , S_y , S_z after sensitivity corrections of the 20 x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} .

After acquiring the amplified output values S_x , S_y , S_z after sensitivity corrections of the x-axis Hall element H_{Ex} , y-axis Hall element H_{Ey} and z-axis Hall element H_{Ez} , 10 values 25 each, the offset information calculation section 18 deletes the oldest data from the data buffer, shifts the remaining data and adds the amplified output values S_x , S_y , S_z acquired this time (step S14).

Then, the offset information calculation section 18 decides whether the difference between a maximum value and minimum value of the respective past 10 amplified output values S_x , S_y , S_z after sensitivity corrections of the x-axis Hall element HEx , y-axis Hall element HEy and z-axis Hall element HEz is greater than a predetermined value, for example, about 1/3 of $a0M$ or not (step S15).

When the difference between a maximum value and minimum value obtained in step S15 is equal to or smaller than the predetermined value, the offset information calculation section 18 discards the amplified output values S_x , S_y , S_z acquired this time, goes back to step S12 and newly acquires amplified output values S_{rx} , S_{ry} , S_{rz} of the x-axis Hall element HEx , y-axis Hall element HEy and z-axis Hall element HEz .

On the other hand, when the difference between a maximum value and minimum value obtained in step S15 is greater than the predetermined value, the offset information calculation section 18 estimates the coordinates (C_x, C_y, C_z) of such a reference point $C1$ whose distances from points $P_1(S1x, S1y, S1z)$, $P_2(S2x, S2y, S2z)$, $P_3(S3x, S3y, S3z)$, ... in which the 10 amplified output values S_x , S_y , S_z correspond to xyz components respectively become as equal as possible (step S16).

Next, the offset information calculation section 18 decides whether the difference between the coordinates (C_x, C_y, C_z) of the reference point $C1$ estimated this time and the coordinates (C_x, C_y, C_z) of the reference point $C1$ estimated last time is smaller than a predetermined value, for example, about $a0M$ or not (step S17), discards the coordinates $(C_x,$

Cy, Cz) of the reference point C1 estimated this time if it is equal to or greater than the predetermined value, goes back to step S12 and newly acquires amplified output values Srx, Sry, Srz of the x-axis Hall element HEx, y-axis Hall element HEy and z-axis Hall element HEz.

On the other hand, when the difference between the coordinates (Cx, Cy, Cz) of the reference point C1 estimated this time and the coordinates (Cx, Cy, Cz) of the reference point C1 estimated last time is smaller than the predetermined value, the offset information calculation section 18 causes the offset information storage section 19a to store the x, y, z components of the coordinates (Cx, Cy, Cz) of the reference point C1 estimated this time as the offset Cx of the x-axis Hall element HEx, offset Cy of the y-axis Hall element HEy and offset Cz of the z-axis Hall element HEz (step S18).

The above described embodiment assumes that the azimuth measuring device is incorporated in the portable device, but it is also possible to accommodate the azimuth measuring device in a case which can be inserted into or detached from a portable device such as a PDA (Personal Digital Assistant) or notebook personal computer and use this azimuth measuring device mounted in the portable device.

For example, it is possible to provide the azimuth measuring device, its data processing IC and interface IC, etc., in a PCMCIA card inserted in a PC card slot provided as standard for a notebook personal computer and incorporate the above-described calibration function as a driver.

The PC card slot has a standard for mechanical and electrical characteristics but has no magnetic characteristic such as leakage flux density inside the slot, and therefore the azimuth measuring device provided inside a general-purpose PCMCIA card cannot predict leakage flux density generated in the notebook personal computer beforehand.

Here, by incorporating the calibration function of the azimuth measuring device in the PCMCIA card, it is possible to accurately correct an offset of the azimuth measuring device even when the leakage magnetic field of the PC card slot varies from one portable device to another and freely mount and use the azimuth measuring device without being limited to a specific portable device.

In the PCMCIA card, it is also possible to mount a tilt sensor, signal processing IC of a GPS (Global Positioning System) and antenna together with the azimuth measuring device and the card format is not limited to the PCMCIA card and may also be made adaptable to a CF card slot.

Furthermore, the above described embodiment has described the case where Hall elements are used as magnetic sensors as an example, but the magnetic sensors are not limited to Hall elements and flux gate sensors, etc., may also be used.

In the above described embodiment, the offset information calculation section 18 is constructed so as to estimate the coordinates of a reference point in such a way that when amplified output values S_x , S_y , S_z are arranged on an xyz coordinate system as points representing x, y, z components respectively, distances of the reference point from the

respective points become as equal as possible, but the present invention is not limited to this and the offset information calculation section 18 may also be adapted so as to estimate the coordinates of a reference point in such a way that in the case where the rates of variation of the amplified output values S_x , S_y , S_z are all equal to or greater than a predetermined value, for example, about $1/3$ of a_0M , the amplified output values S_x , S_y , S_z are arranged on an xyz coordinate system as points representing x, y, z components, the distances of the reference point from the respective points become as equal as possible, and when one of the amplified output values S_x , S_y , S_z has a minimum rate of variation and when the rate of variation of that amplified output value is equal to or smaller than a predetermined value, the offset information calculation section 18 may also be adapted so as to estimate the coordinates of a reference point in such a way that when the amplified output values of other than that having the minimum rate of variation out of the amplified output values S_x , S_y , S_z are arranged on an xy coordinate system as points representing x, y components respectively, the distances from the respective points become as equal as possible.

As a specific method of calculating the rates of variations of amplified output value S_x , S_y , S_z , a calculation of standard deviation, calculation of a difference between a maximum value and minimum value, etc., may be used.

Thus, even when the azimuth measuring device is moved or rotated only on a plane perpendicular to any one of three axes of the three-axis magnetic sensor 11, it is possible to

estimate the coordinates of a reference point relatively accurately.

Furthermore, the above described embodiment is constructed in such a way that it is decided in steps S7, S17 whether a difference between the coordinates (Cx, Cy, Cz) of the reference point C1 estimated this time and the coordinates (Cx, Cy, Cz) of the reference point C1 estimated last time is smaller than a predetermined value or not, but the present invention is not limited to this and the present invention may also be adapted so as to compare the coordinates (Cx, Cy, Cz) of the reference point C1 estimated this time with the coordinates (Cx, Cy, Cz) of a plurality of reference points C1 estimated last time and before last time. More specifically, variations of a predetermined number of reference points C1 estimated latest (including reference point C1 estimated this time) are calculated and the calculated degrees of variations are decided. There may be various methods for calculating variations such as calculating a difference between a maximum value and minimum value of those reference points C1, calculating a standard deviation of those reference points C1, calculating an average of reference points C1 estimated until last time and calculating a difference between the reference points C1 estimated this time and the average, etc. Thus, using a plurality of past estimated values for the coordinates of a reference point C1 can further improve the accuracy.

Furthermore, the above described embodiment has not particularly referred to displaying the acceptability of

offset information, but the present invention is not limited to this and may also be adapted so as to display the acceptability of offset information on the display section 202. More specifically, the degree of acceptability of offset information is classified into a plurality of categories such as excellent, good and fair. Then, focused on a predetermined number of reference points C1 estimated latest (including reference point C1 estimated this time), variations of those reference points C1 are calculated, the reference point C1 estimated this time is classified into any one of categories according to the calculated degree of variations, acceptability information indicating the acceptability corresponding to the category is created and the degree of acceptability of the offset information is displayed on the display section 202 based on the acceptability information created.

Here, the aforementioned method can be used to use a plurality of past estimated values of the coordinates of reference points C1.

This allows the user to recognize the acceptability of offset information with reference to the degree of acceptability displayed.

Furthermore, in the above described embodiment, it is possible to calculate the distances from S_x , S_y , S_z data $P_1(S_{1x}, S_{1y}, S_{1z})$, $P_2(S_{2x}, S_{2y}, S_{2z})$, $P_3(S_{3x}, S_{3y}, S_{3z})$, ... repeatedly acquired in Figure 3 to the estimated reference point C1, decide whether the calculated distance is outside a predetermined range, for example, smaller than $1/2$ of a_{0M} or greater than

1.5 times a0M or not, and discard the output data if the calculated distance is outside the predetermined range. The distance can also be calculated from Formula (28) above using the following formula:

$$5 \quad r = \sqrt{\frac{1}{N} \sum \{(s_{i_x} - c_x)^2 + (s_{i_y} - c_y)^2 + (s_{i_z} - c_z)^2\}} \quad (38)$$

Thus, when a static external environment magnetic field exists or earth magnetism is shielded, it is possible to prevent azimuth from being measured despite the fact that earth magnetism has not been detected correctly.

10 Furthermore, the above described embodiment can also be adapted so as to display reliability of the azimuth measurement result on the display section 202. More specifically, the reliability of the azimuth measurement result is divided into a plurality of categories such as excellent, good and fair.

15 Then, the distances from points $P_1 (S1x, S1y, S1z)$, $P_2 (S2x, S2y, S2z)$, $P_3 (S3x, S3y, S3z)$, ... to the coordinates (C_x, C_y, C_z) of the reference point C1 are calculated, the calculated distances are compared with a plurality of thresholds, classified into any one of categories, reliability information

20 showing the degree of reliability corresponding to the category is created and the degree of reliability of the azimuth measurement result is displayed on the display section 202 based on the reliability information created.

This allows the user to recognize the reliability of the

25 azimuth measurement result with reference to the degree of reliability displayed.

The above described embodiment has described the case of the azimuth measuring device having 3-axis earth magnetism detection means, but the present invention is not limited to this and the present invention is also applicable to an azimuth
5 measuring device having 2-axis earth magnetism detection means as shown in Figure 5.

In this case, a block diagram showing a schematic structure of the azimuth measuring device, a figure illustrating the concept of the azimuth measuring method for an offset value
10 and a flow chart of offset calibration are as shown in Figure 6 to 8.

Furthermore, in the case of the azimuth measuring device having 3-axis earth magnetism detection means, the orientation of the portable device 201 is arbitrarily changed in a
15 three-dimensional space and the amplified output value S_x of the x-axis Hall element HE_x , amplified output value S_y of the y-axis Hall element HE_y and amplified output value S_z of the z-axis Hall element HE_z are acquired repeatedly in the meantime, but in the case of the azimuth measuring device having 2-axis
20 earth magnetism detection means, the orientation of the portable device 101 is changed while keeping the earth magnetism detection directions of two axes on a predetermined plane and the amplified output value S_x of the x-axis Hall element HE_x and amplified output value S_y of the y-axis Hall
25 element HE_y are acquired repeatedly in the meantime. By replacing Formulas (14) to (37) above by Formulas (39) to (58) shown below, the present invention can be applied likewise.

$$\sqrt{M_x^2 + M_y^2} = \text{const} \quad (39)$$

$$r = a_0 \sqrt{M_x^2 + M_y^2} \quad (40)$$

$$(S_x - C_x)^2 + (S_y - C_y)^2 = r^2 \quad (41)$$

$$d_i = \sqrt{(S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2} \quad (42)$$

$$\begin{aligned} 5 \quad \epsilon_i &= d_i^2 - r^2 \\ &= (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \end{aligned} \quad (43)$$

$$\begin{aligned} S &= \sum \epsilon_i^2 \\ &= \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \}^2 \end{aligned} \quad (44)$$

$$\frac{\partial S}{\partial C_x} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \} (S_{i_x} - C_x) \quad (45)$$

$$\frac{\partial S}{\partial C_y} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \} (S_{i_y} - C_y) \quad (46)$$

$$\frac{\partial S}{\partial r} = -4 \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \} \quad (47)$$

$$10 \quad \sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \} (S_{i_x} - C_x) = 0 \quad (48)$$

$$\sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 - r^2 \} (S_{i_y} - C_y) = 0 \quad (49)$$

$$\sum \{ (S_{i_x} - C_x)^2 + (S_{i_y} - C_y)^2 \} - N r^2 = 0 \quad (50)$$

$$r^2 = \frac{1}{N} \sum \{ (Si_x - C_x)^2 + (Si_y - C_y)^2 \} \quad (51)$$

$$C_x \sum Si_x (Si_x - \bar{S}_x) + C_y \sum Si_y (Si_x - \bar{S}_x) = \frac{1}{2} \sum (Si_x^2 + Si_y^2) (Si_x - \bar{S}_x) \quad (52)$$

$$C_x \sum Si_x (Si_y - \bar{S}_y) + C_y \sum Si_y (Si_y - \bar{S}_y) = \frac{1}{2} \sum (Si_x^2 + Si_y^2) (Si_y - \bar{S}_y) \quad (53)$$

$$\bar{S}_x = \frac{1}{N} \sum Si_x \quad (54)$$

$$\bar{S}_y = \frac{1}{N} \sum Si_y \quad (55)$$

$$\begin{bmatrix} \sum Si_x (Si_x - \bar{S}_x) & \sum Si_y (Si_x - \bar{S}_x) \\ \sum Si_x (Si_y - \bar{S}_y) & \sum Si_y (Si_y - \bar{S}_y) \end{bmatrix} \begin{bmatrix} C_x \\ C_y \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sum (Si_x^2 + Si_y^2) (Si_x - \bar{S}_x) \\ \sum (Si_x^2 + Si_y^2) (Si_y - \bar{S}_y) \end{bmatrix} \quad (56)$$

$$\begin{bmatrix} \sum Si_x (Si_x - \bar{S}_x) & \sum Si_y (Si_x - \bar{S}_x) \\ \sum Si_y (Si_x - \bar{S}_x) & \sum Si_y (Si_y - \bar{S}_y) \end{bmatrix} \begin{bmatrix} C_x \\ C_y \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sum (Si_x^2 + Si_y^2) (Si_x - \bar{S}_x) \\ \sum (Si_x^2 + Si_y^2) (Si_y - \bar{S}_y) \end{bmatrix} \quad (57)$$

$$\begin{bmatrix} \sum Si_x^2 - N\bar{S}_x^2 & \sum Si_x Si_y - N\bar{S}_x \bar{S}_y \\ \sum Si_x Si_y - N\bar{S}_x \bar{S}_y & \sum Si_y^2 - N\bar{S}_y^2 \end{bmatrix} \begin{bmatrix} C_x \\ C_y \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sum (Si_x^2 + Si_y^2) (Si_x - \bar{S}_x) \\ \sum (Si_x^2 + Si_y^2) (Si_y - \bar{S}_y) \end{bmatrix} \quad (58)$$

Furthermore, when a reference point C2 is estimated by solving the simultaneous linear equations shown in Formulas (56), (57) or (58), increasing the number of data pieces acquired eliminates the necessity for uniformly orienting the portable device 101 which calibrates offset values in all directions and the orientation of the portable device 101 may be limited within a range of about 180° to 90°. By replacing Formula (38) by Formula (59) below, the present invention can be applied likewise.

$$r = \sqrt{\frac{1}{N} \sum \{ (Si_x - C_x)^2 + (Si_y - C_y)^2 \}} \quad (59)$$

In acquiring the Sx, Sy, Sz data, the above described embodiment repeats data acquisition unconditionally until the

number of data pieces acquired reaches a predetermined value.
However, it is also possible to calculate a difference between
the Sx, Sy, Sz data acquired immediately before every time
the Sx, Sy, Sz data is acquired and discard the acquired Sx,
5 Sy, Sz data when the difference is smaller than the
predetermined value.

Thus, even when a state in which the orientation of the
portable device hardly changes during calibration continues,
it is possible to prevent wrong offset values from being
10 calculated causing inappropriate offset corrections to be
carried out.

Figure 9 shows an example of the Sx, Sy, Sz data acquired
when the orientation of the portable device is changing
appropriately and all data is changing with time. On the other
15 hand, Figure 10 shows an example of the Sx, Sy, Sz data acquired
when the orientation of the portable device hardly changes
and all data remains substantially constant.

In the case of the Sx, Sy, Sz data shown in Figure 10,
the difference between the maximum value and minimum value
20 of the Sx, Sy, Sz data is decided to be equal to or below a
predetermined value in step S15 in the offset calibration flow
chart shown in Figure 4, and therefore the process does not
move to the step of estimating a reference point.

However, when the orientation of the portable device
25 changes only for a short time while the Sx, Sy, Sz data is
being acquired, the Sx, Sy, Sz data becomes as shown in Figure
11 and parts whose values change appear. In this case, in
step S15, the difference between the maximum value and minimum

value of the Sx, Sy, Sz data may be decided to be greater than a predetermined value and the process may move to the step of estimating a reference point. This causes a considerably large error to occur in estimating the reference point with
5 the result that wrong offset values are calculated.

Therefore, by calculating difference from the Sx, Sy, Sz data acquired immediately before every time the Sx, Sy, Sz data is acquired and discarding the Sx, Sy, Sz data when the difference is smaller than a predetermined value, it is
10 possible to prevent reference points from being estimated with inappropriate Sx, Sy, Sz data because the acquired Sx, Sy, Sz data is discarded as long as the orientation of the portable device hardly changes.

There may be various specific methods of calculating
15 differences of Sx, Sy, Sz data and deciding whether or not to discard the data, for example, calculating a difference for each piece of the Sx, Sy, Sz data and discarding the Sx, Sy, Sz data if all the differences do not exceed a predetermined value or calculating the sum of squares of respective
20 differences of the Sx, Sy, Sz data and discarding the Sx, Sy, Sz data when the result does not exceed the predetermined value.

Industrial Applicability

As described above, according to the azimuth measuring
25 device according to claims 1 to 12 or the azimuth measuring method according to claims 13 to 20, it is possible to calculate offset information with respect to the output of each axis of the magnetism detection means by only arbitrarily changing

the orientation of the portable device, simplify the offset calibration work and reduce load on the user when carrying out offset calibration.